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**To whom it may concern**

Sub: **New ISO/CD 15016 Example**  
here: **Re-evaluation according to  
the proposed rational method**  
Ref.: Evaluations ISO\_fin4 to \_fin9.mcd  
and EVEREST\_04 to \_08.mcd

The present re-evaluation of the new ISO/CD 15016 example includes **the reduction to the no-wind and no-waves condition** according to the rational method. **In order to obtain the maximum size of the sample and to avoid the impression that data have been excluded purposely the data of all ten runs have been included.**

Following systematic scrutiny of the data during the former evaluations the power during the third run,  $i = 2$ , has been changed from 11349 kW to 11549 kW. Maybe there has been a misprint in the data at some stage?

Values computed according to the rational procedure are plotted in red, results of the full sample denoted by boxes, where appropriate. The values taken from ISO/CD 15016 are plotted in blue and denoted by circles.

<b>Units</b>	kN := $10^3 \cdot \text{newton}$	N := newton	
		W := watt	
<b>Constants</b>	Field strength	$g := 9.81 \cdot \text{m} \cdot \text{sec}^{-2}$	$g := \frac{g}{\text{m} \cdot \text{sec}^{-2}}$
<b>Test identification</b>	TID := "23010"	New ISO/CD 15016 example	
<b>Constants</b>	Length of ship	$L := 318 \cdot \text{m}$	$L := \frac{L}{\text{m}}$
	Diameter of propeller	$D := 9.5 \cdot \text{m}$	$D := \frac{D}{\text{m}}$
	Density of sea water	$\rho := 1.024 \cdot 10^3 \cdot \text{kg} \cdot \text{m}^{-3}$	$\rho := \frac{\rho}{\text{kg} \cdot \text{m}^{-3}}$
	Density of air	$\rho_A := 1.225 \cdot \text{kg} \cdot \text{m}^{-3}$	$\rho_A := \frac{\rho_A}{\text{kg} \cdot \text{m}^{-3}}$

## Functions and subroutines

### Normalise data

$$JH(V, N) := \frac{V}{D \cdot N}$$

$$KP(P, N) := \frac{P}{\rho \cdot D^5 \cdot N^3}$$

$$Fn(V) := \frac{V}{\sqrt{g \cdot L}}$$

$$CP(P, V) := \frac{P}{\rho \cdot D^2 \cdot V^3}$$

### Basic functions

$$PS(p, N, V) := p_0 \cdot N^3 + p_1 \cdot N^2 \cdot V$$

### Sort runs

```
Sort(JH, KP, ψ) :=
  j0 ← 0
  j1 ← 0
  for i ∈ 0..last(JH)
    if ψi > π
      Sj0,0 ← JHi
      Sj0,1 ← KPi
      j0 ← j0 + 1
    otherwise
      Sj1,2 ← JHi
      Sj1,3 ← KPi
      j1 ← j1 + 1
  S
```

### Compute left-inverse

```
LeftInv(A) :=
  r ← rows(A)
  c ← cols(A)
  s ← svds(A)
  for i ∈ 0..c - 1
    ISVi,i ← (si)-1
  UV ← svd(A)
  U ← submatrix(UV, 0, r - 1, 0, c - 1)
  V ← submatrix(UV, r, r + c - 1, 0, c - 1)
  Ainv ← V · ISV · UT
  Ainv
```

### Solve cubic equations

$$\text{Revs}(p, V, P, N) := \left| \begin{array}{l} n_i \leftarrow \text{last}(V) \\ \text{for } i \in 0..n_i \\ \quad \left| \begin{array}{l} q_0 \leftarrow P_i \\ q_1 \leftarrow V_i \\ n \leftarrow N_i \\ N_{\text{rat}_i} \leftarrow \text{root}(q_0 - p_0 \cdot n^3 - p_1 \cdot n^2 \cdot q_1, n) \end{array} \right. \\ N_{\text{rat}} \end{array} \right.$$

### Analyse power supplied

$$\text{Supplied}(D, \rho, t, \psi_0, V_G, n, P) := \left| \begin{array}{l} \text{for } i \in 0.. \text{last}(t) \\ \quad \left| \begin{array}{l} A_{\text{sup}_{i,0}} \leftarrow (n_i)^3 \\ A_{\text{sup}_{i,1}} \leftarrow (n_i)^2 \cdot V_{G_i} \\ d_{\text{FM}_i} \leftarrow \text{if}(\psi_0 < \pi, -1, 1) \\ A_{\text{sup}_{i,2}} \leftarrow (n_i)^2 \cdot d_{\text{FM}_i} \\ \text{for } j \in 3..5 \\ \quad A_{\text{sup}_{i,j}} \leftarrow A_{\text{sup}_{i,2}} \cdot (t_i)^{j-2} \end{array} \right. \\ X_{\text{sup}} \leftarrow \text{LeftInv}(A_{\text{sup}}) \cdot P \\ E_{\text{sup}} \leftarrow P - A_{\text{sup}} \cdot X_{\text{sup}} \\ p_0 \leftarrow X_{\text{sup}_0} \\ p_1 \leftarrow X_{\text{sup}_1} \\ \text{for } j \in 0..3 \\ \quad v_j \leftarrow \frac{X_{\text{sup}_{2+j}}}{X_{\text{sup}_1}} \\ \text{for } i \in 0.. \text{last}(t) \\ \quad \left| \begin{array}{l} V_{\text{F.rat}_i} \leftarrow \sum_{j=0}^3 v_j \cdot (t_i)^j \\ V_{\text{S0.rat}_i} \leftarrow V_{G_i} + V_{\text{F.rat}_i} \cdot d_{\text{FM}_i} \end{array} \right. \end{array} \right.$$

$$\left[ \begin{array}{l} P_{S.rat_i} \leftarrow PS(p, n_i, V_{S0.rat_i}) \\ J_{H.rat_i} \leftarrow JH(V_{S0.rat_i}, n_i) \\ K_{P.rat_i} \leftarrow KP(P_{S.rat_i}, n_i) \end{array} \right] \left[ E_{sup} \quad V_{F.rat} \quad V_{S0.rat} \quad P_{S.rat} \quad J_{H.rat} \quad K_{P.rat} \quad p \quad v \right]$$

### Analyse power required

$$\text{Required}(V_{S0}, P_S, Env) := \left[ \begin{array}{l} V_{WindR} \leftarrow (Env_{0,0})_{0,0} \\ \Psi_{WindR} \leftarrow (Env_{0,0})_{0,1} \\ V_{SeasR} \leftarrow (Env_{0,1})_{0,0} \\ \Psi_{SeasR} \leftarrow (Env_{0,1})_{0,1} \\ H_{Seas} \leftarrow (Env_{0,1})_{0,2} \\ V_{SwellR} \leftarrow (Env_{0,2})_{0,0} \\ \Psi_{SwellR} \leftarrow (Env_{0,2})_{0,1} \\ H_{Swell} \leftarrow (Env_{0,2})_{0,2} \\ \text{for } i \in 0..last(V_{S0}) \\ \quad \left[ \begin{array}{l} \text{for } j \in 0..2 \\ \quad A_{req_{i,0}} \leftarrow (V_{S0_i})^{j+1} \\ \quad V_{WindR.x_i} \leftarrow V_{WindR_i} \cdot \cos(\Psi_{WindR_i}) \\ \quad A_{req_{i,3}} \leftarrow V_{WindR.x_i} \cdot V_{WindR_i} \cdot V_{S0_i} \\ \quad V_{SeasR.x_i} \leftarrow V_{SeasR_i} \cdot \cos(\Psi_{SeasR_i}) \\ \quad A_{req_{i,4}} \leftarrow (H_{Seas_i})^2 \cdot V_{SeasR.x_i} \cdot V_{SeasR_i} \cdot V_{S0_i} \\ \quad V_{SwellR.x_i} \leftarrow V_{SwellR_i} \cdot \cos(\Psi_{SwellR_i}) \\ \quad A_{req_{i,5}} \leftarrow (H_{Swell_i})^2 \cdot V_{SwellR.x_i} \cdot V_{SwellR_i} \cdot V_{S0_i} \end{array} \right] \\ X_{req} \leftarrow \text{LeftInv}(A_{req}) \cdot P_S \\ E_{req} \leftarrow P_S - A_{req} \cdot X_{req} \\ P_{AWind} \leftarrow A_{req}^{<3>} \cdot X_{req_3} \\ P_{ASeas} \leftarrow A_{req}^{<4>} \cdot X_{req_4} \end{array} \right]$$

$$\begin{aligned}
 & P_{ASwell} \leftarrow A_{req}^{<5>} \cdot X_{req_5} \\
 & P_{AWaves} \leftarrow P_{ASeas} + P_{ASwell} \\
 & \text{for } i \in 0..last(V_{S0}) \\
 & \quad P_{AAir_i} \leftarrow (V_{S0_i})^3 \cdot X_{req_3} \\
 & P_{S0} \leftarrow P_S - P_{AWaves} - P_{AWind} + P_{AAir} \\
 & [E_{req} \ P_{AWind} \ P_{AWaves} \ P_{S0}]
 \end{aligned}$$

### Compute relative wave motion

$$\begin{aligned}
 \text{Relative}(V_G, T, \psi) := & \text{for } i \in 0..last(V_G) \\
 & V \leftarrow \frac{g \cdot T_i}{2 \cdot \pi} \\
 & V_{Rx} \leftarrow V_{G_i} + V \cdot \cos(\pi + \psi_i) \\
 & V_{Ry} \leftarrow V \cdot \sin(\pi + \psi_i) \\
 & V_{R_i} \leftarrow \sqrt{V_{Rx}^2 + V_{Ry}^2} \\
 & \psi_{R_i} \leftarrow \text{angle}(V_{Rx}, V_{Ry}) \\
 & [V_R \ \psi_R]
 \end{aligned}$$

### Power supplied

Data reported from traditional trial measurements

time:	course:	speed over ground:	rate of revolution:	shaft power
row 48	row 3	row 4	row 5	row 6
$t := \begin{bmatrix} 16.792 \\ 18.830 \\ 20.826 \\ 23.053 \\ 24.986 \\ 26.682 \\ 30.597 \\ 32.433 \\ 34.231 \\ 35.849 \end{bmatrix}$	$\psi_0 := \begin{bmatrix} 5.901 \\ 2.909 \\ 5.901 \\ 2.909 \\ 5.901 \\ 2.909 \\ 2.909 \\ 5.901 \\ 2.909 \\ 5.901 \end{bmatrix}$	$V_G := \begin{bmatrix} 4.409 \\ 5.561 \\ 6.050 \\ 7.182 \\ 7.218 \\ 8.082 \\ 8.416 \\ 7.773 \\ 8.437 \\ 7.922 \end{bmatrix}$	$n := \begin{bmatrix} 0.7317 \\ 0.7300 \\ 0.9267 \\ 0.9267 \\ 1.0467 \\ 1.0467 \\ 1.0933 \\ 1.0950 \\ 1.1167 \\ 1.1133 \end{bmatrix}$	$P_S := \begin{bmatrix} 5711 \\ 5533 \\ 11349 \\ 11140 \\ 16200 \\ 16190 \\ 18500 \\ 18330 \\ 19450 \\ 19756 \end{bmatrix}$
	·hr	·rad	$\frac{m}{sec}$	·Hz
				·kW

$P_{S_2} := 11549 \cdot \text{kW}$       **This value is being modified!**

Data non-dimensionalized in view of further use in some mathematical subroutines,  
which by definition cannot handle arguments with (different) dimensions

$$t := \frac{t}{\text{hr}} \quad \psi_0 := \frac{\psi_0}{\text{rad}} \quad V_G := \frac{V_G}{\text{m} \cdot \text{sec}^{-1}} \quad n := \frac{n}{\text{Hz}} \quad P_S := \frac{P_S}{\text{W}}$$

$t_m := \text{mean}(t)$        $t := t - t_m$

**Normalised data**

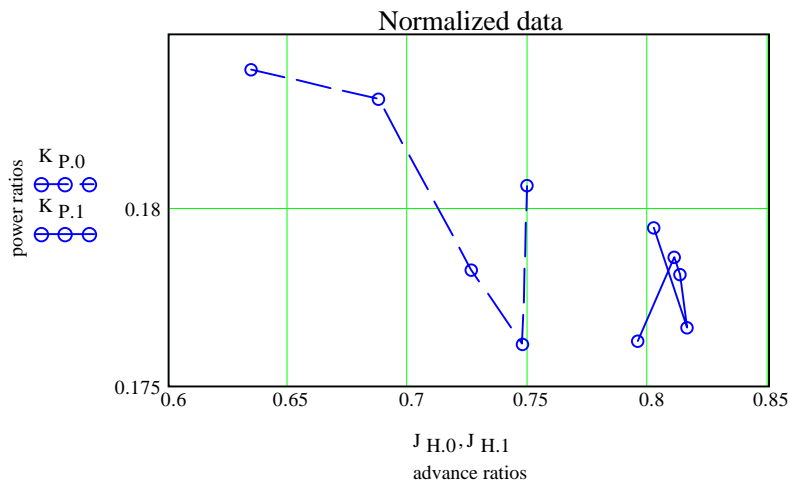
$i := 0 .. \text{last}(t)$

$J_{H_i} := JH(V_{G_i}, n_i)$        $K_{P_i} := KP(P_{S_i}, n_i)$

**First check of consistency**

$J_{H.0} := \text{Sort}(J_H, K_P, \psi_0)^{<0>}$        $K_{P.0} := \text{Sort}(J_H, K_P, \psi_0)^{<1>}$

$J_{H.1} := \text{Sort}(J_H, K_P, \psi_0)^{<2>}$        $K_{P.1} := \text{Sort}(J_H, K_P, \psi_0)^{<3>}$



**Input data for statistical analysis:  
all possible subsets of nine runs**

$i := 0 .. \text{last}(t)$

$j := 0 .. \text{last}(t) - 1$

$K_{j,i} := \text{if}(j < i, j, j + 1)$

$t_{S_{j,i}} := t_{K_{j,i}}$        $\psi_{OS_{j,i}} := \psi_{0_{K_{j,i}}}$        $V_{GS_{j,i}} := V_{G_{K_{j,i}}}$        $n_{S_{j,i}} := n_{K_{j,i}}$        $P_{SS_{j,i}} := P_{S_{K_{j,i}}}$

**Evaluation**

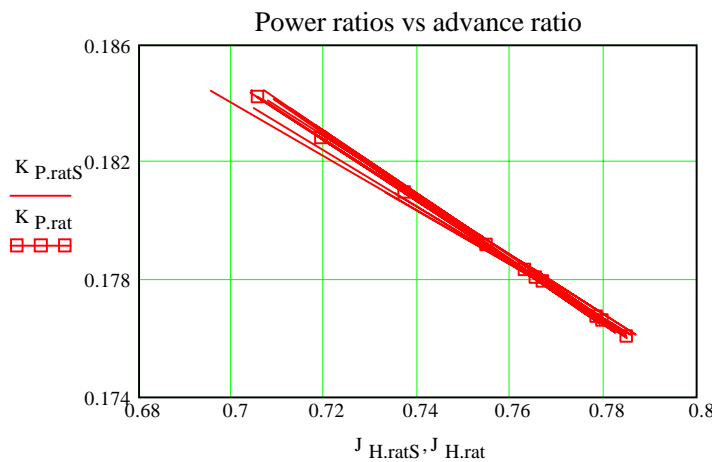
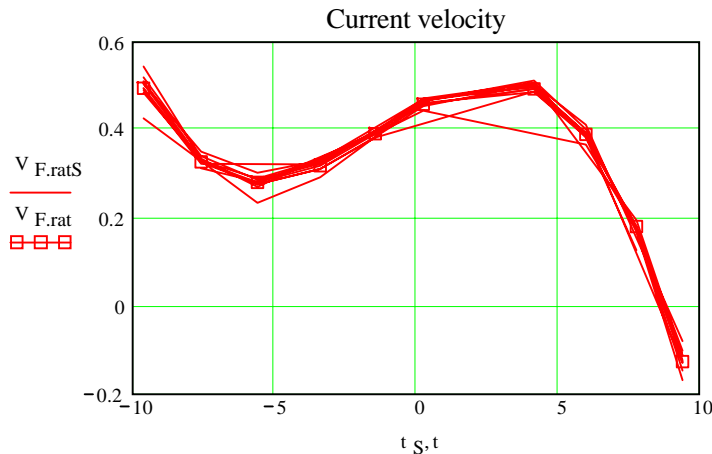
$\text{Res}_{\text{sup}S_i} := \text{Supplied}(D, \rho, t_S^{<i>}, \psi_{OS}^{<i>}, V_{GS}^{<i>}, n_S^{<i>}, P_{SS}^{<i>})$

$$\left[ E^{<i>} \quad V_{F.ratS}^{<i>} \quad V^{<i>} \quad P^{<i>} \quad J_{H.ratS}^{<i>} \quad K_{P.ratS}^{<i>} \quad P_{ratS}^{<i>} \quad v_{ratS}^{<i>} \right] := Res_{supS_i}$$

$$Res_{sup} := Supplied(D, \rho, t, \psi_0, V_G, n, P_S)$$

$$\left[ E_{sup} \quad V_{F.rat} \quad V_{S.rat} \quad P_{S.rat} \quad J_{H.rat} \quad K_{P.rat} \quad P_{rat} \quad v_{rat} \right] := Res_{sup}$$

### Second check of consistency



These two results of all possible subsets of nine runs show, that after correction of the 'misprint' the data are consistent.

### Interpolations

$$m := 36$$

$$k := 0..m$$

$$t_{rat_k} := \min(t) + \frac{(\max(t) - \min(t))}{m} \cdot k$$

$$V_{F.rat_k} := \sum_{l=0}^3 v_{rat_1} \cdot (t_{rat_k})^l$$

$$J_{H.rat_i} := JH(V_{S.rat_i}, n_i)$$

## Final performance data according to ISO evaluation

frequency of revolution:  
row 61 (5)

$$n_{0.ISO} := \begin{bmatrix} 0.7317 \\ 0.7300 \\ 0.9267 \\ 0.9267 \\ 1.0467 \\ 1.0467 \\ 1.0933 \\ 1.0950 \\ 1.1167 \\ 1.1133 \end{bmatrix} \cdot \text{Hz}$$

ship speed:  
row 65

$$V_{S0.ISO} := \begin{bmatrix} 5.230 \\ 5.238 \\ 6.852 \\ 6.861 \\ 7.932 \\ 7.946 \\ 8.315 \\ 8.327 \\ 8.501 \\ 8.480 \end{bmatrix} \cdot \frac{\text{m}}{\text{sec}}$$

brake power:  
row 63

$$P_{S0.ISO} := \begin{bmatrix} 5331 \\ 5293 \\ 10839 \\ 10838 \\ 15582 \\ 15578 \\ 17945 \\ 17696 \\ 18606 \\ 19022 \end{bmatrix} \cdot \text{kW}$$

Non-dimensional values, not normalized(!), in coherent units

$$n_{0.ISO} := \frac{n_{0.ISO}}{\text{Hz}}$$

$$V_{S0.ISO} := \frac{V_{S0.ISO}}{\text{m} \cdot \text{sec}^{-1}}$$

$$P_{S0.ISO} := \frac{P_{S0.ISO}}{\text{W}}$$

Normalised values

$$i := 0 .. \text{last}(n_{0.ISO})$$

$$J_{H0.ISO_i} := JH(V_{S0.ISO_i}, n_{0.ISO_i})$$

$$K_{P0.ISO_i} := KP(P_{S0.ISO_i}, n_{0.ISO_i})$$

### ISO/CD results:

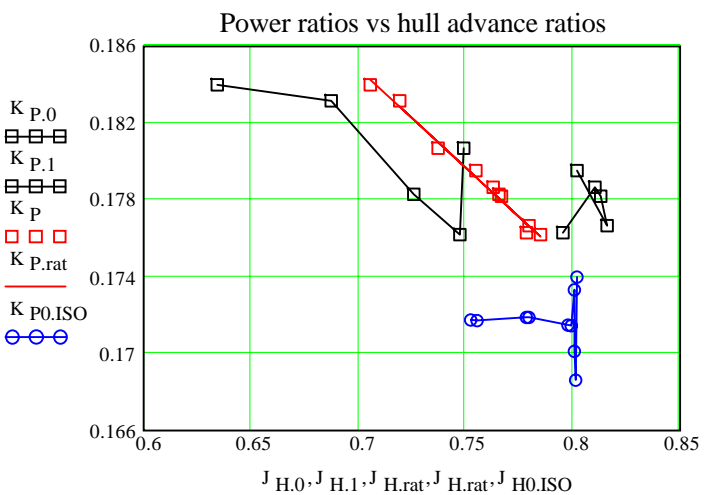
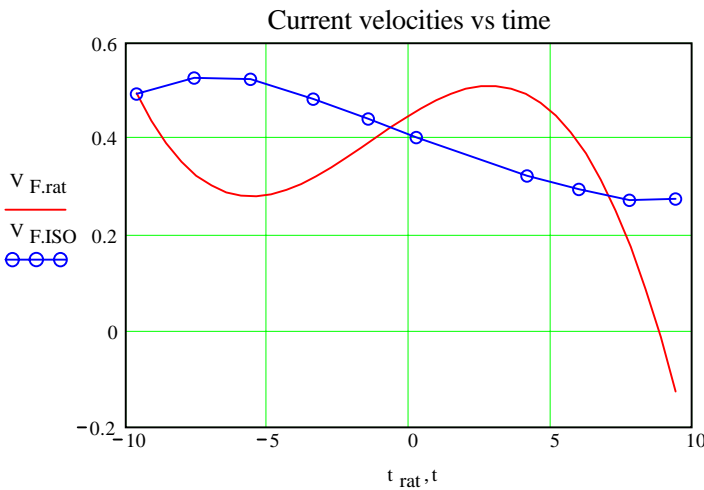
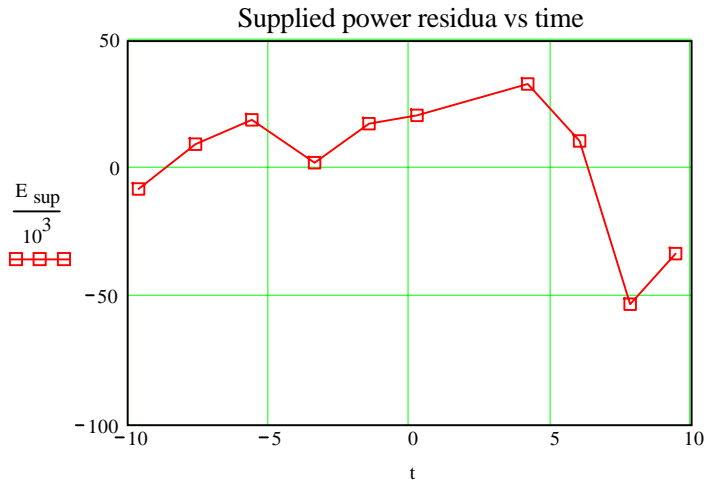
current at each run:  
row 52

$$V_{F.ISO} := \begin{bmatrix} 0.494 \\ 0.527 \\ 0.525 \\ 0.484 \\ 0.442 \\ 0.404 \\ 0.324 \\ 0.296 \\ 0.273 \\ 0.275 \end{bmatrix} \cdot \frac{\text{m}}{\text{sec}}$$

$$V_{F.ISO} := \frac{V_{F.ISO}}{\text{m} \cdot \text{sec}^{-1}}$$



**Plots of results**



**Attention!** At this stage the power has not yet been reduced to the no wind and no wave conditon in the rational evaluation while it has been reduced in the traditional evaluation! But these results already show, that the results according to the proposed ISO procedure are outside the law of the shaft power.

## Power required

### Relative wind measured

relative wind velocity:  
row 7

$$V_{\text{WindR}} := \begin{bmatrix} 13.5 \\ 4.0 \\ 15.0 \\ 2.8 \\ 16.0 \\ 0.7 \\ 0.4 \\ 16.5 \\ 0.0 \\ 16.5 \end{bmatrix} \cdot \frac{\text{m}}{\text{sec}}$$

relative wind direction:  
row 8

$$\Psi_{\text{WindR}} := \begin{bmatrix} -0.1745 \\ 2.5307 \\ -0.1745 \\ 2.3562 \\ 0.0873 \\ 2.6180 \\ 2.3562 \\ 0.0873 \\ 2.5307 \\ -0.1745 \end{bmatrix} \cdot \text{rad}$$

**Non-dimensional values, not normalized(!), in coherent units**

$$V_{\text{WindR}} := \frac{V_{\text{WindR}}}{\text{m} \cdot \text{sec}^{-1}}$$

$$\Psi_{\text{WindR}} := \frac{\Psi_{\text{WindR}}}{\text{rad}}$$

### Sea state observed

mean wave period (seas)  
row 12

$$T_{\text{Seas}} := \begin{bmatrix} 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 3.90 \\ 2.80 \\ 2.80 \\ 2.80 \\ 2.80 \end{bmatrix} \cdot \text{sec}$$

significant wave height (seas) incident angle of wave (seas)  
row 13

$$H_{\text{Seas}} := \begin{bmatrix} 1.00 \\ 1.00 \\ 1.00 \\ 1.00 \\ 1.00 \\ 1.00 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \end{bmatrix} \cdot \text{m}$$

row 14

$$\Psi_{\text{Seas}} := \begin{bmatrix} 2.97 \\ -0.17 \\ 2.97 \\ -0.17 \\ 2.97 \\ -0.17 \\ -0.17 \\ 2.97 \\ -0.17 \\ 2.97 \end{bmatrix}$$

$$T_{\text{Seas}} := \frac{T_{\text{Seas}}}{\text{sec}}$$

$$H_{\text{Seas}} := \frac{H_{\text{Seas}}}{\text{m}}$$

$$\begin{bmatrix} V_{\text{SeasR}} & \Psi_{\text{SeasR}} \end{bmatrix} := \text{Relative}(V_G, T_{\text{Seas}}, \Psi_{\text{Seas}})$$

### Swell state observed

mean wave period (swell)  
row 15

$$T_{\text{Swell}} := \begin{bmatrix} 10.59 \\ 10.59 \\ 10.59 \\ 10.59 \\ 11.32 \\ 11.32 \\ 11.32 \\ 11.32 \\ 11.32 \\ 11.32 \\ 11.32 \end{bmatrix} \cdot \text{sec}$$

$$T_{\text{Swell}} := \frac{T_{\text{Swell}}}{\text{sec}}$$

significant wave height (swell) incident angle of wave (swell)  
row 16

$$H_{\text{Swell}} := \begin{bmatrix} 2.00 \\ 2.00 \\ 2.00 \\ 2.00 \\ 2.50 \\ 2.50 \\ 2.50 \\ 2.50 \\ 2.50 \\ 3.00 \\ 3.00 \end{bmatrix} \cdot \text{m}$$

$$H_{\text{Swell}} := \frac{H_{\text{Swell}}}{\text{m}}$$

$$\Psi_{\text{Swell}} := \begin{bmatrix} 0.6981 \\ -2.4435 \\ 0.6981 \\ -2.4435 \\ 0.6981 \\ -2.4435 \\ -2.4435 \\ 0.6981 \\ -2.4435 \\ 0.6981 \end{bmatrix}$$

$$\begin{bmatrix} V_{\text{SwellR}} & \Psi_{\text{SwellR}} \end{bmatrix} := \text{Relative}(V_G, T_{\text{Swell}}, \Psi_{\text{Swell}})$$

### Input data for statistical analysis

$$\text{Wind} := \begin{bmatrix} V_{\text{WindR}} & \Psi_{\text{WindR}} \end{bmatrix}$$

$$\text{Seas} := \begin{bmatrix} V_{\text{SeasR}} & \Psi_{\text{SeasR}} & H_{\text{Seas}} \end{bmatrix}$$

$$\text{Swell} := \begin{bmatrix} V_{\text{SwellR}} & \Psi_{\text{SwellR}} & H_{\text{Swell}} \end{bmatrix}$$

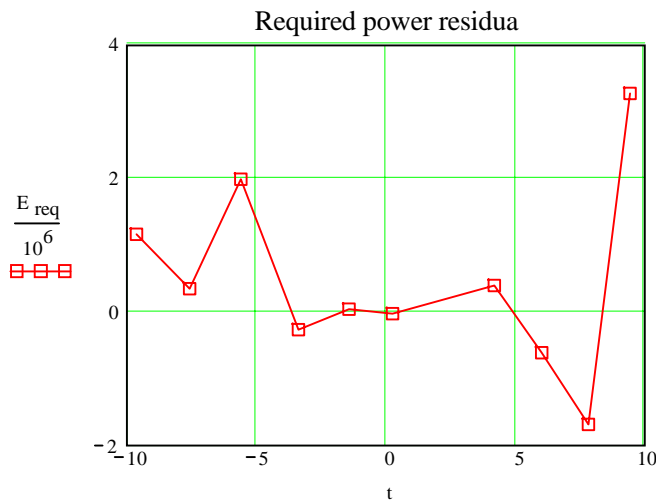
$$\text{Env} := (\text{Wind} \ \text{Seas} \ \text{Swell})$$

### Evaluation

$$\text{Res}_{\text{req}} := \text{Required}(V_{\text{S.rat}}, P_{\text{S}}, \text{Env})$$

$$\begin{bmatrix} E_{\text{req}} & P_{\text{AWind.rat}} & P_{\text{AWaves.rat}} & P_{\text{S.rat}} \end{bmatrix} := \text{Res}_{\text{req}}$$

**Plots of results**  
**Power residua**



After six runs the trials had to be stopped for a while in view of the large swell height due to the passing of a typhoon!

**Additional power and resistance due to wind according to ISO/CD evaluation**

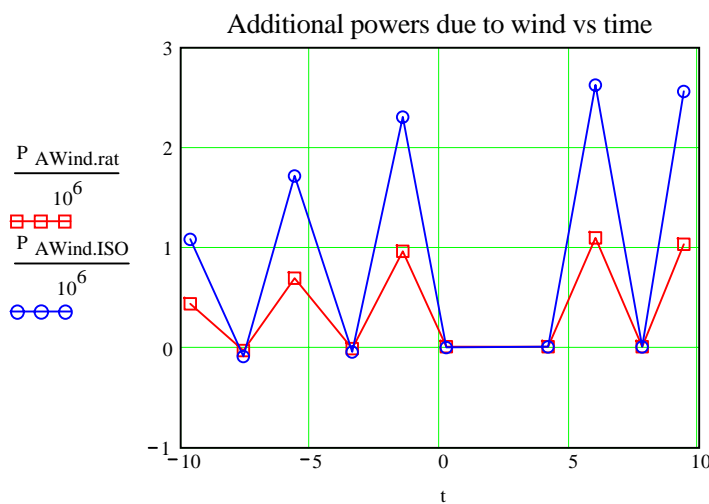
$\eta_D := 0.6$  Propulsive efficiency, crude estimate for plausibility checks only!

$$R_{AWind.ISO} := \frac{R_{AWind.ISO}}{N}$$

$$P_{AWind.ISO_i} := \frac{R_{AWind.ISO_i} \cdot V_{S.rat_i}}{\eta_D}$$

resistance increase due to wind row 29:

$$R_{AWind.ISO} := \begin{bmatrix} 131.5 \\ -10.9 \\ 162.3 \\ -4.5 \\ 181.2 \\ -0.3 \\ -0.1 \\ 192.7 \\ 0 \\ 196.5 \end{bmatrix} \cdot 10^3 \cdot N$$



$$\left| \frac{P_{AWind.rat}}{P_{AWind.ISO}} \right| = 0.409$$

**Additional power and resistance due to waves**

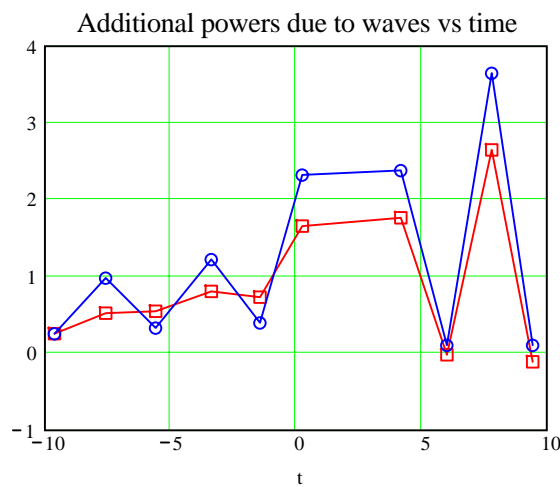
**according to ISO/CD evaluation**

resistance increase due to waves  
row 30:

$$R_{AWaves.ISO} := \frac{R_{AWaves.ISO}}{N}$$

$$P_{AWaves.ISO_i} := \frac{R_{AWaves.ISO_i} \cdot V_{S.rat_i}}{\eta_D}$$

$$R_{AWaves.ISO} := \begin{bmatrix} 31.4 \\ 111.8 \\ 31.4 \\ 106.9 \\ 31.4 \\ 182.6 \\ 180.1 \\ 7.9 \\ 264.7 \\ 7.9 \end{bmatrix} \cdot 10^3 \cdot N$$



$$\frac{|P_{AWaves.rat}|}{|P_{AWaves.ISO}|} = 0.736$$

**Fairing**

i := 0..last(t) - 3      j := 0..3      cubic 'spline'!

$$A_{i,j} := (V_{S.rat_i})^j      B_i := P_{S.rat_i}$$

$$X := \text{LeftInv}(A) \cdot B$$

**Interpolating**

$$V_{S0.rat_k} := \min(V_{S.rat}) + \frac{\max(V_{S.rat}) - \min(V_{S.rat})}{m} \cdot k$$

$$A_{k,j} := (V_{S0.rat_k})^j$$

$$P_{S0.rat} := A \cdot X$$

n\_rat\_k := 1      initial values

Actually only runs 8 and 9 needed to be disregarded!

## Final performance

### Final performance data according to rational evaluation

$$n_{0.rat} := \text{Revs}(p_{rat}, V_{S0.rat}, P_{S0.rat}, n_{rat})$$

### Normalized values

#### Advance ratios, power ratios

$$J_{H0.rat_k} := JH(V_{S0.rat_k}, n_{0.rat_k})$$

$$K_{P0k.rat_k} := KP(P_{S0.rat_k}, n_{0.rat_k})$$

$$p := 0..1$$

$$J_{H0.rat_0} := \min(J_{H0.rat})$$

$$K_{P0.rat_0} := \max(K_{P0k.rat})$$

$$J_{H0.rat_1} := \max(J_{H0.rat})$$

$$K_{P0.rat_1} := \min(K_{P0k.rat})$$

$$J_{H0.ISO_i} := JH(V_{S0.ISO_i}, n_{0.ISO_i})$$

$$K_{P0.ISO_i} := KP(P_{S0.ISO_i}, n_{0.ISO_i})$$

#### Froude numbers, power numbers

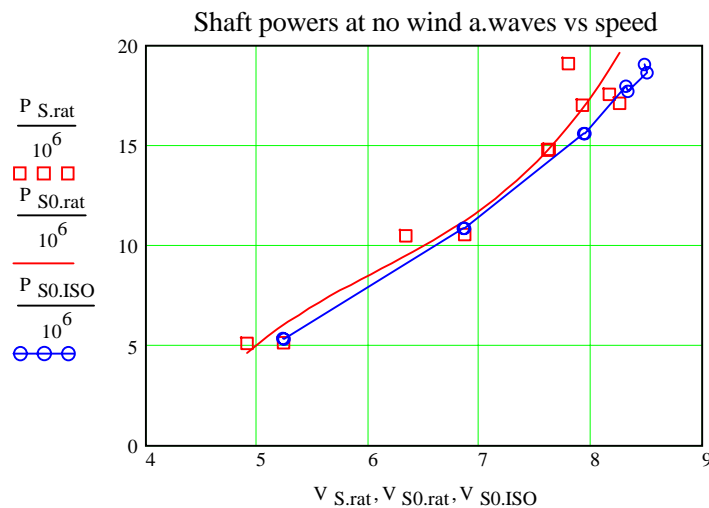
$$F_{n0.rat_k} := Fn(V_{S0.rat_k})$$

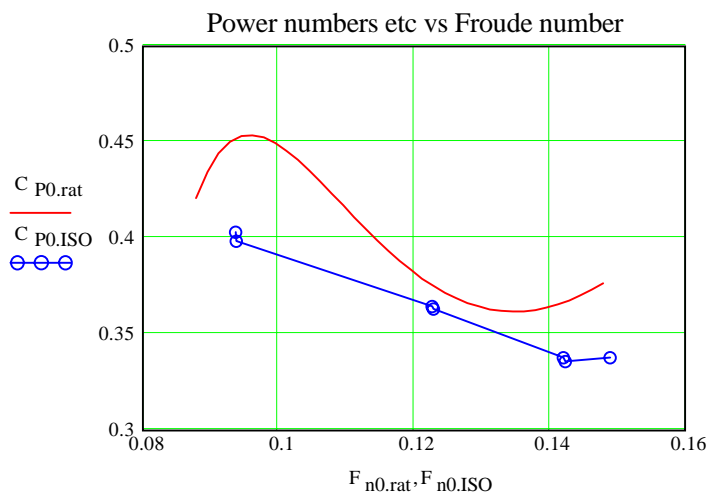
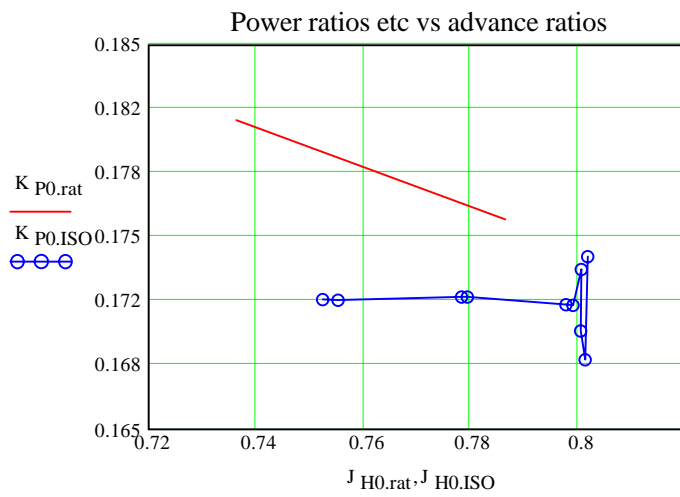
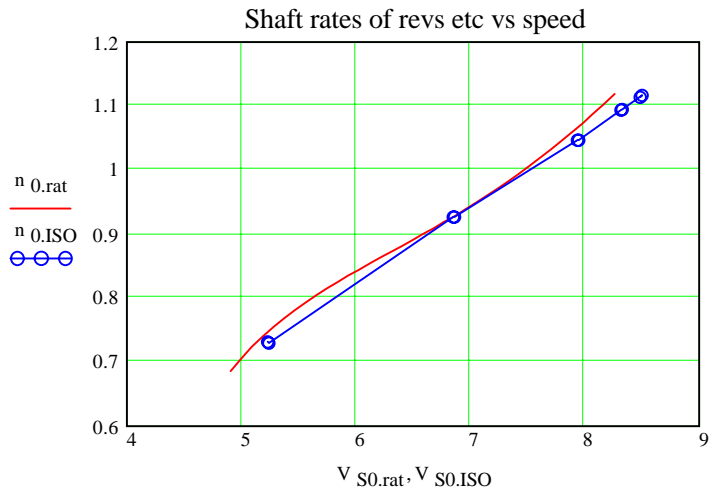
$$C_{P0.rat_k} := CP(P_{S0.rat_k}, V_{S0.rat_k})$$

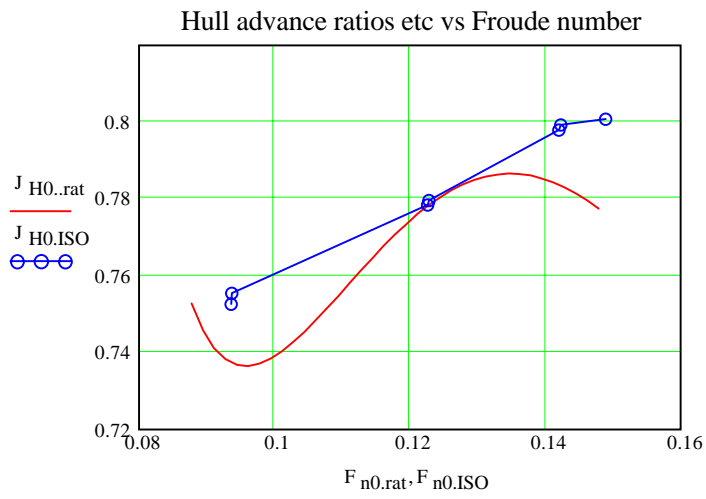
$$F_{n0.ISO_i} := Fn(V_{S0.ISO_i})$$

$$C_{P0.ISO_i} := CP(P_{S0.ISO_i}, V_{S0.ISO_i})$$

### Plots of final results







**END Rational re-evaluation of new ISO/CD 15016 example**

Fr Mrz 02 20:20:20 2001

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